

MULTISPECTRAL HIGH FIDELITY RADAR SCENE GENERATOR

PROGRAM PROGRESS REPORT SBIR PHASE I; TOPIC N99-059

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Prepared for:

Government Technical Liaison
Naval Air Systems Command, Headquarters
Attn: Mr. James Evans, Bldg. 2272
Suite 535, Code PMA 272
Patuxent River, MD 20670

Prepared by:

Anand Kelkar
Malibu Research Associates
26670 Agoura Rd.
Calabasas, CA 91302

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Malibu Research

26670 Agoura Road
Calabasas, CA 91302-1974
(818) 880-5494 Fax 880-5499

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Malibu Research

26670 Agoura Road
Calabasas, CA 91302-1974

<http://www.MalibuResearch.com>

This is the third monthly progress report for the Multispectral High Fidelity RADAR Scene Generator SBIR (Phase I), Contract # N68335-99-C-0126.

1.0 Work Summary

Work that was done between Apr. 12 and May. 12 included some of the items that were intended to be addressed in the previous reporting period. The real time RADAR interface contribution into the RADAR Scene Generator (RSG) was defined and the connection points for all the interface attributes were identified. Additionally, circuit diagrams for a real time version of the RSG were developed. The RSG is able to be implemented as a desktop analytical simulator as well as a real time RADAR interactive device. The desktop analytical simulator can be run on a standard PC and is therefore uninteresting from a hardware configuration standpoint. The real time model has computational constraints placed on it as well as interactivity requirements that demand attention at the microsecond level. This is where the hardware interconnection speeds and data transfer rates are directly responsible for performance. This report covers the tradeoff space that was investigated and the resulting configuration.

2.0 Schedule

As anticipated in the proposal, a full schematic of the real-time RSG implementation has been developed. The RADAR specific portion of the RSG has been left for definition when a specific target RADAR has been picked.

3.0 Studies

An effective interface for real-time RSG implementation was developed. This consists of 2 portions... (1) signals to the RADAR and (2) signals from the RADAR.

RSG signals to RADAR

When attached to a RADAR, the RSG has to be able to interact with the signal processor and selected portions of the receiver chain. The most convenient place to interact is one where the interconnections are minimized. This approach tends to affect existing hardware to the least degree.

All RADARs have an intermediate frequency (IF) where the matched filtering takes place. This IF consists of the real time RADAR data downconverted for handling convenience. In the case of modern RADARs, this IF is often directly digitized so as to avoid the pitfalls of in-phase (I) and quadrature (Q) channel imbalance that has to be maintained in the receiver chain. The baseband conversion is then done in the digital domain where signal purity can be maintained more easily.

The nature of RSG signal generation requires that there be individually controllable I & Q components involved to create the composite signal seen by the RADAR. Conceptually, the easiest interface to the RADAR is at the digital level where the I & Q components are still pristine. However, the data bandwidth associated with such a connection makes it impractical. For example, the digital data bandwidth is determined by the maximum signal bandwidth, and in the case of the example chosen in the first progress report, the hypothetical RADAR has a 10 MHz "wideband" mode used for precision tracking. The 10 MHz would imply that I & Q samples had to be injected at a 10 MSPS rate, where each sample was 2 bytes wide (16 bit resolution usually covers the most stringent application).

This means that a 40 MBPS data channel has to be provided along with all the synchronizing signals in order to test such a RADAR. The implementation for such an information channel requires that the RSG be in close proximity to the RADAR signal processor (typically 6 ft. or less) or that there be provisions for re-synchronizing hardware at various points along the way. Further, that signal processor boards in the RADAR be modified to accept an alternate source for such broadband digital data... for each channel of a multi-channel RADAR.

This is where IF injection proves to be the most practical approach. In the case of a multi-channel RADAR, each receive channel has just 1 IF connection (usually co-axial) associated. On the RSG end this means digital-IF conversion, but this step allows the RSG to be compatible with virtually all RADARs in the field. Prudent design of the IF conversion hardware would provide the complex RADAR signal(s) at a nominal IF frequency. Further, the IF conversion unit would be the synchronizer that coordinated the RSG output with the RADAR clocks. Each RADAR application would have associated a frequency converter designed to tailor the RSG output to a coherent reference signal provided by the RADAR.

Control signals from RADAR

The RSG is required to interact with the RADAR on a real time basis. To so do, a set of control signals are required from the RADAR:

Time synchrony – These are the set of signals that will be required to synchronize the RADAR operations with the RSG.

Main bang – signal representing the trigger to the RADAR transmitter. This signal will be fed to the digital-to-IF conversion hardware so that it can "play back" its buffer, which has been loaded by the digital processor portion of the RSG.

Command data transfer – this signal consists of a set of apriori data (protocol TBD) that originates in the “beam scheduler” (or equivalent) portion of the RADAR. This data describes the settings for the antenna (if it is a phased array) and any other equipment in preparation for the next measurement interval. The expected apriori margin at this point is approximately 3 msec. Depending on the RADAR, this set of signals can range from the very simple... such as a frequency code for a continuous azimuth search RADAR... to the other extreme where the RADAR dynamically selects waveforms, STC contours, processing bandwidths, transmit power levels and antenna beam positions.

Status information back to the RADAR – most modern RADARs have continuous monitoring of the command data stream to the hardware. In the situation that the integrity of this data link is compromised, the RADAR reports a catastrophic fault and usually aborts its mission.

Digitizing clock – used by the A/D to synchronize the live data collection process. This signal is fed directly to the digital-to-IF conversion hardware where it is used to clock out the digital data buffer. As a result of the apriori RADAR settings, the RSG digital hardware has filled the data buffer in the IF conversion device.

Antenna synchrony. The beam position commands have been addressed in the “command data transfer” section above. Some RADARs have dynamic selection of antenna aperture weights for various mission dictated modes. The RSG requires this specific information so the appropriate sidelobe contributions (in various EW modes) or the changing beamwidths (in precision track modes) can be correctly reflected in the live data.

Processing synchrony – this set of interfaces coordinates the RSG output with the signal processor state. For example, some RADARs have wideband precision track modes where a “track gate” has been established around the target, and all the processing resources have been focused to this track gate to maximize the fidelity of the process. The same principles apply to the RSG. With the apriori knowledge of this track gate, the RSG can abandon the rest of the range trace and focus its processing resources on processing wide band clutter models within the track gate only, resulting in higher fidelity environment emulation.

RSG hardware tradeoff issues.

There is a variety of signal processor hardware available on the market. After performing an initial survey of the market, the field of qualifying candidates was:

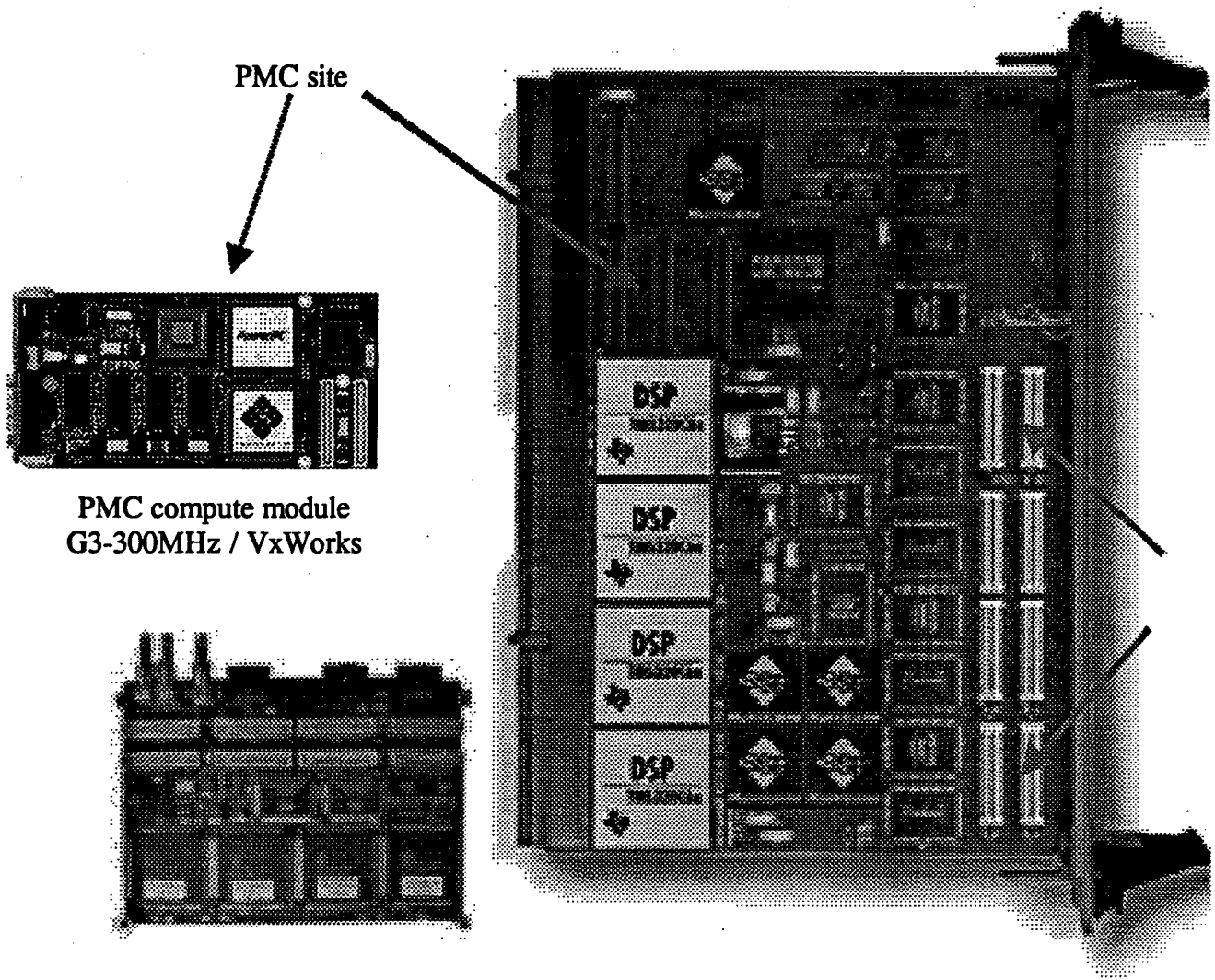
Octagon Systems in Westminster, Colorado – embedded PC solutions
Eonic Systems in Herndon, Virginia – real-time DSP and RISC solutions
Alta Technology in Sandy, Utah – parallel networking applications
Motorola in El Segundo, California – Power PC networked processors
Acromag in Wixom, Michigan – Industrial I/O solutions for VME and cPCI

Spectrum Signal Processing in Burnaby, BC, Canada – real-time DSP for VME & cPCI
Pentek in Upper Saddle River, NJ – DSP & data acquisition for a variety of data buses
CSPI in Billerica, Massachusetts – multi processor compute nodes

Some of the issues that were considered in arriving at a recommended solution were:

- 1) Hardware maturity – what was available on the market, how long the architecture had been fielded, what the bus infrastructure was & where it was migrating and what role the vendor had in providing a working solution (rather than a group of parts mounted on a board).
- 2) Software development environment – maturity, ease of use, code portability and integration with other development environments. Typically, the DSP has a set of unique software tools that have to integrate with an overall development platform such as Unix, Windows, DOS etc.
- 3) Tech Support availability – time zone compatibility for voice support, and additional forums for other forms of tech support... E-mail, Web site, Bulletin board etc...
- 4) Compatibility with existing Malibu Research RES (RADAR Environment Simulator) code – Malibu Research has produced many high fidelity target generating environments for RADARs in the past. The RSG development cost would be greatly reduced if the code development cycle could be foreshortened by using existing modules developed for various incarnations of the RES.

Hardware Approach for the RSG



The hardware COTS configuration that best addresses the requirements of the RSG (faster speed is better) and is consistent with the 4 guidelines indicated is shown above. There is one Canadian company that potentially provides a complete hardware solution for the RSG... Spectrum Signal Processing Inc. in Burnaby, British Columbia.

The TMS320-C6X processor was the engine that was selected. This Texas Instruments product has a basic 1.6 GIPs (Giga-instruction/sec) benchmark for the floating point product, which is due to hit the COTS market in 6/99. The pin compatible integer version of this product is supported by Spectrum Signal Processing Inc. at present with a family of available boards ranging from a single processor board to the quad processor board shown above. These family of boards support the industry standard PMC (PCI Mezzanine Card) site which allows addition of a general purpose processor board (Power PC G3 or G4 being the most likely candidate) with a wide bus bandwidth (132 MB/s) interconnect. Also, there are proprietary PEM (Processor Expansion Module) sites available on the board to allow direct plug in of the IF conversion hardware at even a higher data bandwidth (400 MB/s). When the floating point silicon becomes available, the same family of boards and software tools are expected to handle the development since the floating point processor is an on-chip upgrade.

The RSG tradespace has no hard boundaries. Signal fidelity is the figure of merit. The assessment of required compute power has been made based on the advertised benchmarks for FFT processes and arithmetic computations in the floating point version of the TI DSP processor (66 μ S for a 1024 point complex FFT and 5 nS for a complex multiply/add). For the RADAR model presented in the first progress report, the longest search ranges (300 Km) require the most compute power.

The approach proposed for the RSG required FFTs to be performed as a means to effect waveform convolution with the live range trace data. After considering all the computations that had to be done to fill the range trace buffer in the IF conversion module, a requirement of 2 TI DSP chips was deemed necessary for each RADAR channel. One chip is capable of providing the range trace for each and every pulse (at a 1 MSPS rate) with approximately 25% margin and the second chip is used to do the scene management calculations with approximately 50% margin. This means that the board shown above will support 2 RADAR channels (of the type described in the first progress report) from a computational standpoint.

Given the 2 processor availability, a prior knowledge of RADAR operation was required to be 3mS in order to preserve the planned fidelity as indicated earlier. This assumed that all the environment generation had been done off-line and existed in a data file. As the 3mS is reduced, the RSG will forego some of the fidelity of the "live" data. For example, most RADARs use the first few pulses to provide "space fill" functions to prime the clutter canceling process. The RSG would use this time to perform the required processing without too much impact on the RADAR. The "space fill" function in the RSG is addressed simply by computing the correct ambiguous range and placing clutter returns accordingly.

At some point, if the live data bandwidth significantly increases for example, the RSG processing will be re-allocated to include the other 2 processors on the board, and then each quad DSP processor board will be able to support a single data channel.

A US based company, Echotek Corp. in Huntsville, AL provides the class of hardware required by the RSG, for the PEM site. In initial conversations, Echotek has indicated willingness to create custom designs for specific applications as would be required by the RSG.

The details of this hardware configuration are as follows:

Processing power:

C6201 (fixed point processor) 1600MIPS @ 200MHz

C6701 (floating point version) same

The quad board identified above contains 4 ea. Of these processors

Data infrastructure:

PEM (Processor Expansion Module) bus: 400MB/s to each C62

Will support - FPDP (Front Panel Data Port) protocol

The IF conversion hardware is planned to be attached to this interface

PMC (PCI Mezzanine Card) bus: 132MB/s
Will support – RACEway & FPDP protocols

Available memory on the quad DSP board:

16MB SDRAM (Synchronous Dynamic RAM) per DSP chip

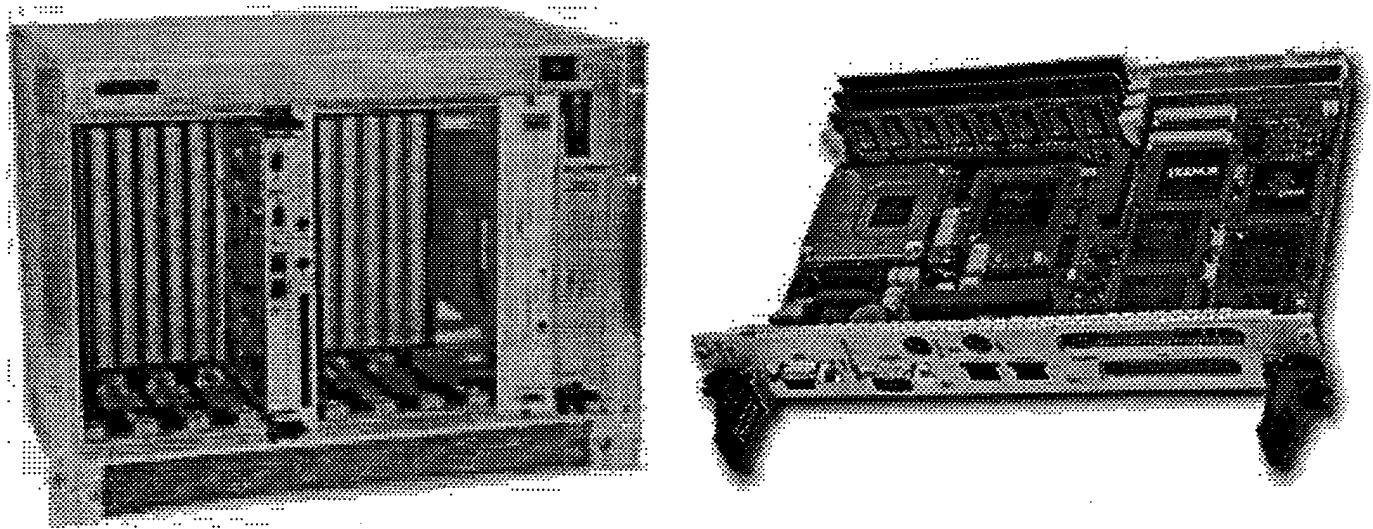
2MB SBSRAM (Synchronous Burst Dynamic RAM) accessible to all DSP chips

Chassis selection:

The VME standard, which has been around for a long time is in the process of being replaced with “Compact PCI (cPCI)”. The implementation of this new approach is similar to the VME in size, however the bus protocol is the same as PCI, which was developed through the Personal Computer market.

There are several chassis manufacturers that provide cPCI chassis solutions for the proposed processor. A local distributor is the most likely vendor choice for this item since the technical complexity of a chassis is minimal and the benefits of having the vendor in close proximity pay large dividends when a problem is encountered.

The proposed chassis is distributed by a local company, “One Stop Systems” and is shown below:



This chassis was chosen with the conscious knowledge that the RSG might require expansion. The maximum available slots (16) was considered a requirement although if a card count is made with the proposed target RADAR (in the 1st progress report), an 8 slot chassis will suffice.

The card shown installed in the center of the chassis is the host PC computer which will be required for the User interface portion of the RSG. This PC host also serves as a bridge

between the 2 halves of the chassis which is fabricated as 2 individual 8 slot sub-chassis components... also for maximum flexibility.

Details of the chassis selection are presented below:

- Rack mount enclosure with fans

- [1] 350 watt modular power supply

- 16-slot cPCI backplane with rear I/P support

- 300MHz Pentium II CPU board, including:

 - bridge interface between the 2 halves of the overall chassis

 - 128 MB SDRAM

 - VGA, keyboard, mouse, Com1 & ethernet connectors on face plate

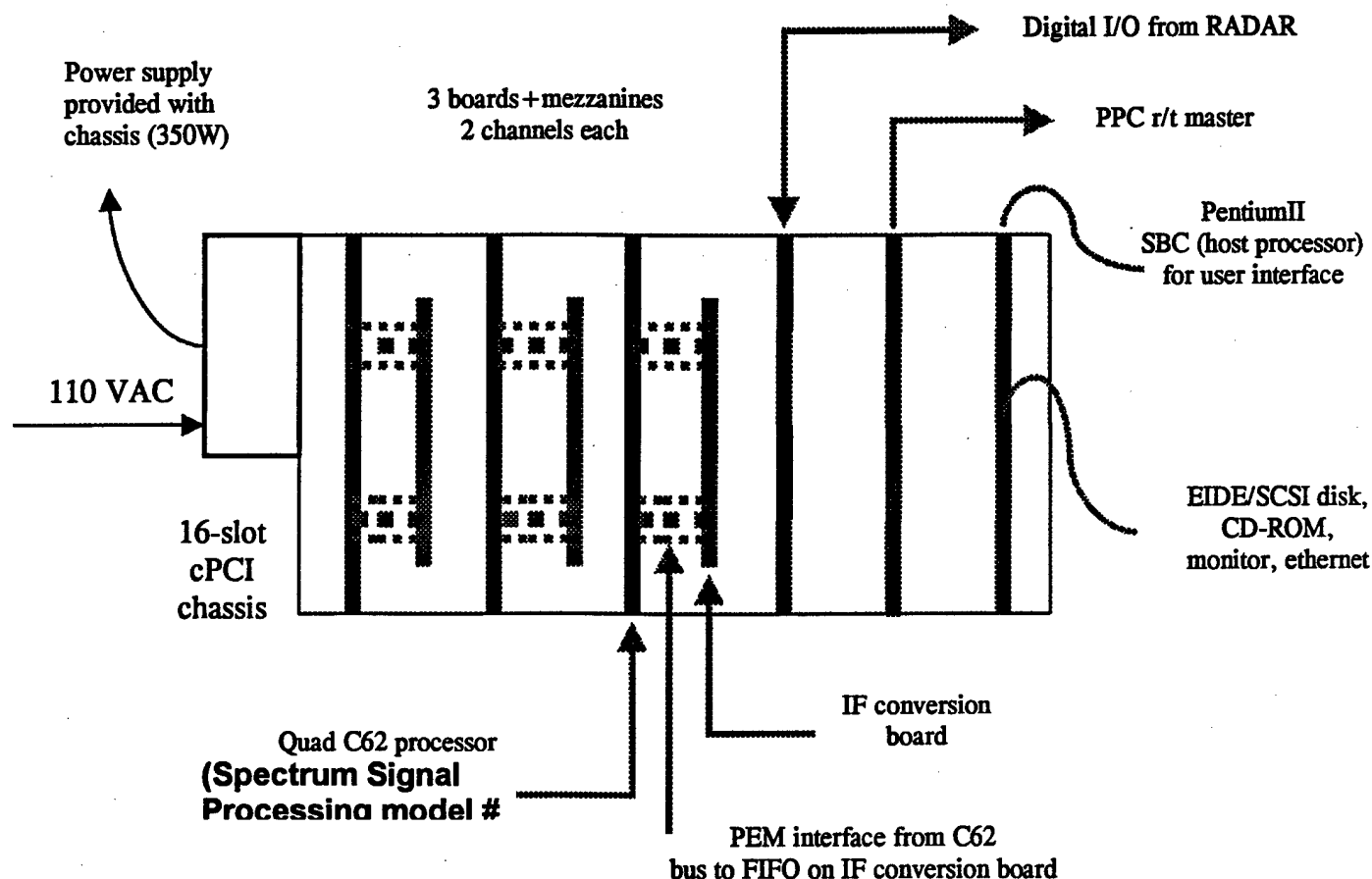
 - One PMC interface

- 3.2GB hard disk and floppy drive mezzanine

- 40X CD-ROM drive with vertical holder

- WindowsNT pre-loaded on the hard disk

- Dimensions: 19.0" wide, 15.75" tall, and 11.5" deep



An overall interconnection of the RSG components has been shown above. The components that are indicated can be fully serviced by the 350W power supply that is provided by the chassis manufacturer. 3.3 Volt low power silicon allows a significant reduction in power consumption on the part of the DSP assets, which have traditionally been the power hungry components in real time systems.

A general purpose computer card (Power PC r/t master) was planned into the architecture since the DSP chips are pipelined processors. Their efficiency at context switching operations may preclude the need for the "r/t master" processor which was intended to provide help in the area of scene parameter translation from the database to the range trace portion of the processing chain.

The digital I/O portion of the RSG is intended to provide the command and status interface to the RADAR. As such, this card represents the portion of the RSG that is subject to change depending on the eventual application of the RSG. The overall design approach will be CPLD (Complex Programmable Logic Device) based and will have the anticipated interface to accommodate up to 4 streams of serial data or 32 bit wide parallel transfers.

Up to 6 channels can be supported with the configuration proposed above. The COTS approach allows the various components to be simply plugged together without much overhead. The only variables are the RADAR specific connections.

An overall enclosure to house the RSG is planned and will be addressed in detail in subsequent phases of this SBIR. This overall enclosure will serve as the physical interface between the RADAR connections and the RSG I/O. Interconnections within the RSG will be planned with integration and troubleshooting as a goal, but will be constrained by size. RADAR connections on the other hand are completely defined by the specific RADAR.

3.0 Plan for next month

- a) Document acceptable data interface formats from the various modeling components that contribute to the RSG
- b) Identify potential application (RADAR development, testing, training etc...) and target RADAR where the Malibu Research approach to the RSG may be used.

5.0 Anticipated Problems:

None